

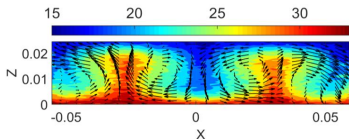
Transition to (spatio-temporal complexity and) turbulence in thermoconvection & aerodynamics

Emmanuel Plaut

How does the flow in a (closed or open) fluid system change from laminar to complex or turbulent as a control parameter is changed ?

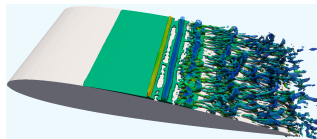
Fluid physics:

part 1: thermoconvection
closed heated fluid systems



[Leclerc & Métivier]

part 2: aerodynamics
open shear flows



[Tangermann & Klein]

Methods:

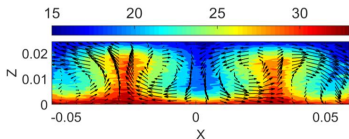
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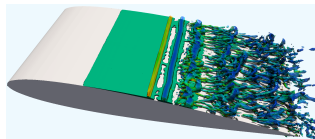
Fluid physics:

part 1: **thermoconvection**
closed heated fluid systems



[Leclerc & Métivier]

part 2: **aerodynamics**
open shear flows



[Tangermann & Klein]

Methods: **linear** then **weakly nonlinear stability analysis**
= **bifurcation theory** or '**catastrophe theory**'

Analytical calculations in part 1 vs numerical computations in part 2

with a 'spectral method'... and Mathematica !

Transition to (spatio-temporal complexity and) turbulence in thermoconvection & aerodynamics

<http://emmanuelplaut.perso.univ-lorraine.fr/t2t>

Session	Date	Content
→ 1 -	29/09	Thermoconvection: phenomena, equations, differentially heated cavity, cavity heated from below = RB cavity, linear stability analysis
2 -	06/10	RB Thermoconvection: linear & weakly nonlinear stability analysis
3 -	13/10	RB Thermoconvection: nonlinear phenomena
4 -	20/10	Aerodynamics of OSF : linear stability analysis
5 -	27/10	Aerodynamics of OSF : linear & weakly nonlinear stability analyses
6 -	10/11	Aerodynamics of OSF : nonlinear phenomena
	24/11	Examination

RB = Rayleigh-Bénard

OSF = Open Shear Flows

Transition to (spatio-temporal complexity and) turbulence in **thermoconvection** & **aerodynamics**

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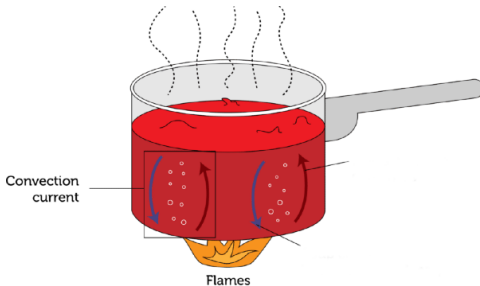
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Follow up module in January & February 2023: **Turbulence & Wind Energy**

<http://emmanuelplaut.perso.univ-lorraine.fr/twe>

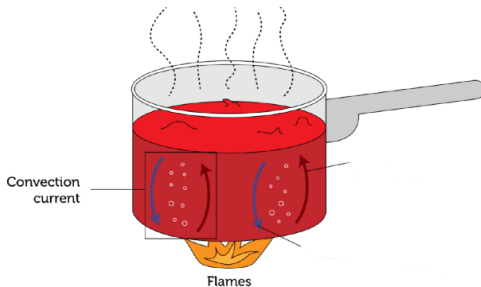
1st part of this module:
Transition to turbulence, or, to spatio-temporal complexity,
in natural thermoconvection

- Fluids in non-isothermal situations
- temperature gradients may drive **natural thermoconvection** = **buoyancy forces** = **heat-driven flows and transfers** !
- This happens in the **kitchen...**



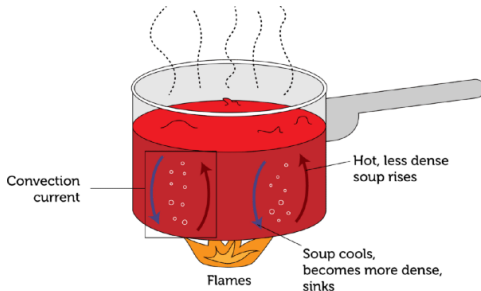
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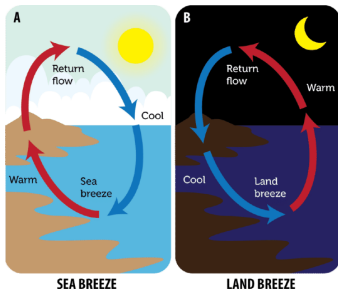
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The question is: **how thermoconvection comes in and develops ?**

or:

how do flows transit to spatial complexity in thermoconvection...

in simpler systems ?

Seeking the answer, we will learn **advanced methods for fluid mechanics !**

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Today - session 1

- **Natural thermoconvection:**
introduction, equations, example of the **differentially heated cavity**
- **Rayleigh-Bénard system = cavity heated from below:**
linear stability analysis with slip boundary conditions

Natural thermoconvection: equations

- Fluids in non-isothermal situations have a density ρ that depends on T

$$\rho = \rho(T) .$$

- If temperature gradients exist, in a gravity field, **buoyancy forces** part of $\rho\mathbf{g}$ may drive **natural thermoconvection**.
- Equations of motion

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- Equations of motion of a **Newtonian fluid**:

$$\rho \frac{d\mathbf{v}}{dt} = \rho[\partial_t \mathbf{v} + (\mathbf{v} \cdot \nabla)\mathbf{v}] = \rho\mathbf{g} - \nabla p + \eta \Delta \mathbf{v} , \quad (\text{NS})$$

$$\partial_t \rho + \text{div}(\rho \mathbf{v}) = 0 , \quad (\text{MC})$$

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with η the dynamic viscosity, κ the heat diffusivity.

Natural thermoconvection: equations

⇒ criterion of existence of hydrostatic conduction solutions ?

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- Hydrostatic conduction solutions:** $\mathbf{v} = \mathbf{0} \implies \nabla T \parallel \mathbf{g}$.

Hence ∇T not vertical \implies **thermoconvection flows always develop**.

Natural thermoconvection: equations under the Oberbeck-Boussinesq approximations

- Fluids in non-isothermal situations have a density ρ that depends on T , under the 1st OB approximation, linearly:

$$\rho = \rho_0 [1 - \alpha(T - T_0)]$$

with ρ_0 the reference density, T_0 the reference temperature,
 α the small thermal expansion coefficient.

- Equations of motion under the **OB approximations**:

$$\rho_0 \frac{d\mathbf{v}}{dt} = \rho_0 [\partial_t \mathbf{v} + (\mathbf{v} \cdot \nabla) \mathbf{v}] = \rho \mathbf{g} - \nabla p + \eta \Delta \mathbf{v}, \quad (\text{NS})$$

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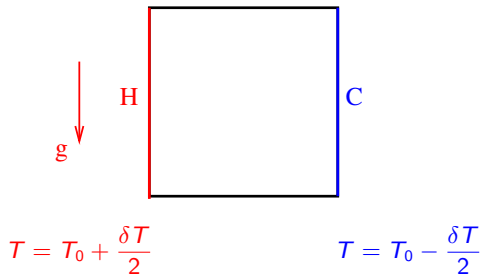
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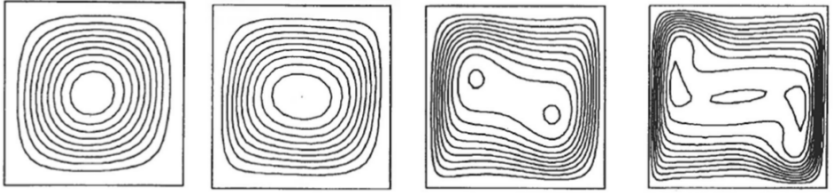
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Thermoconvection in a differentially heated cavity

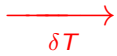
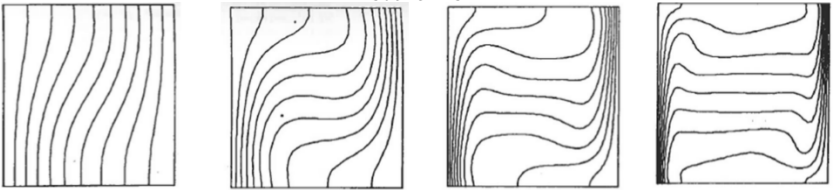


Steady thermoconvection in a 2D differentially heated cavity

Streamlines:



Isotherms:



[De Vahl Davis 1983 Natural convection of air in a square cavity:
A benchmark numerical solution. *Int. J. Num. Meth. Fluids*]

**Main dimensionless control parameter:
dimensionless measure of δT ?**

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OB equations :

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Idea: $R = \frac{\alpha \delta T g}{\nu \Delta v} = \frac{\alpha \delta T g d^2}{\nu V}$ with d the length scale of the cavity.

Determine V taking into account the feedback of \mathbf{v} onto T . Where is this feedback ?

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$$\implies R = \frac{\alpha \delta T \mathbf{g} d^3}{\kappa \nu} \quad \text{Rayleigh number .}$$

Caution: $V = \kappa/d$ meaningful from the point of view of dimensional analysis - not always true regarding orders of magnitude !

Main dimensionless control parameter: Rayleigh number

$$R = \frac{\alpha \delta T g d^3}{\nu \kappa}$$

Order of magnitude for typical fluids ?

Fluid	T_0	thermal expansion coefficient α	kinematic viscosity ν	heat diffusivity κ
Water	20 °C	$2 \cdot 10^{-4} \text{ K}^{-1}$	$1 \cdot 10^{-6} \text{ m}^2/\text{s}$	$1 \cdot 10^{-7} \text{ m}^2/\text{s}$
Air	27 °C		$2 \cdot 10^{-5} \text{ m}^2/\text{s}$	$2 \cdot 10^{-5} \text{ m}^2/\text{s}$

www.engineeringtoolbox.com

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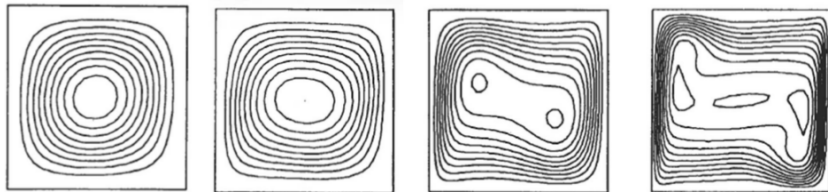
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R large as soon as δT and d not too small !

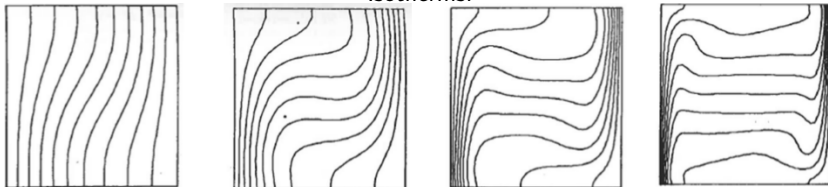
www.engineeringtoolbox.com

Steady thermoconvection in a 2D differentially heated cavity

Streamlines:



Isotherms:



$$R = \frac{\alpha \delta T g d^3}{\kappa \nu} = 10^3$$

$$R = 10^4$$

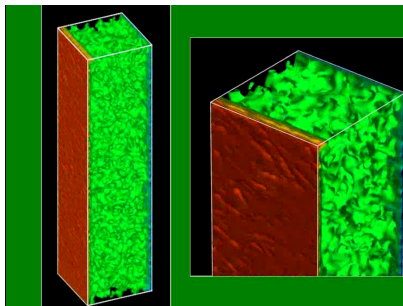
$$R = 10^5$$

$$R = 10^6$$

[De Vahl Davis 1983 Natural convection of air in a square cavity:
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Unsteady thermoconvection in a 3D differentially heated cavity

DNS at $R = 2 \cdot 10^9$, for a height aspect ratio of 4 : initial condition isotherms:

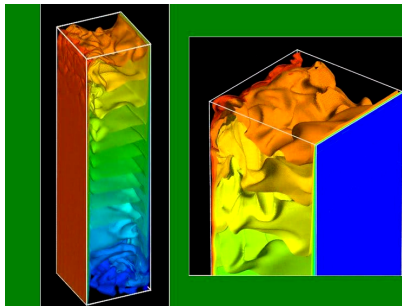


[Trias, Soria et al. 2007 DNS of 2 and 3-dimensional turbulent natural convection flows in a differentially heated cavity of aspect ratio 4. *J. Fluid Mech.*]

www.fxtrias.com/natural_convection.html

Unsteady thermoconvection in a 3D differentially heated cavity

DNS at $R = 2 \cdot 10^9$, for a height aspect ratio of 4 : end-of-the-run isotherms:



[Trias, Soria et al. 2007 DNS of 2 and 3-dimensional turbulent natural convection flows in a differentially heated cavity of aspect ratio 4. *J. Fluid Mech.*]

The isotherms are, in the core of the cavity, roughly horizontal planes...

like in the high- R 2D case of De Vahl Davis, [see frame 14](#) !..

The study of a **simpler 2D system** at $R = 10^6$
gives relevant informations for the **complex 3D system** at $R = 2 \cdot 10^9$!

What we learnt about natural thermoconvection

- It is governed (in 1st approximation) by the **OB equations**:

$$\operatorname{div} \mathbf{v} = 0 , \quad (\text{MC})$$

$$\frac{d\mathbf{v}}{dt} = -\alpha T \mathbf{g} - \nabla p'' + \nu \Delta \mathbf{v} , \quad (\text{NS})$$

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- The main dimensionless control parameter is the **Rayleigh number**

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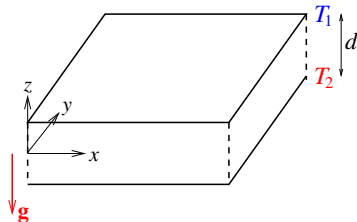
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- The main dimensionless control parameter is the **Rayleigh number**

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- ∇T not vertical \Rightarrow **thermoconvection flows develop at once.**
- ∇T vertical \Rightarrow **thermoconvection flows do not always start ?
how do they start ?**

Study of the Rayleigh-Bénard system: plane cavity heated from below



The OB equations

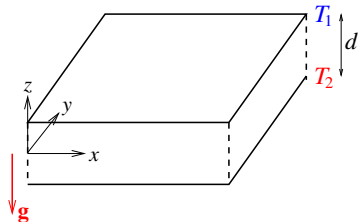
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always admit a **static solution**

Study of the Rayleigh-Bénard system: plane cavity heated from below



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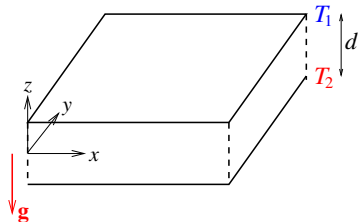
$$\frac{d\mathbf{v}}{dt} = -\alpha T \mathbf{g} - \nabla p'' + \nu \Delta \mathbf{v}, \quad (\text{NS})$$

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always admit a **static solution** that satisfies the isothermal boundary conditions:

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Study of the Rayleigh-Bénard system: plane cavity heated from below



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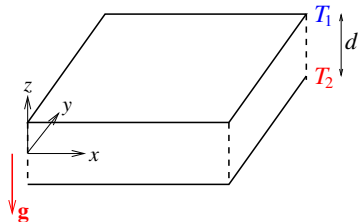
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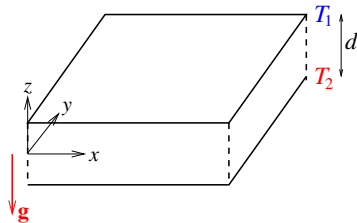
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Thus, how convection can set in ? Through an instability of the static solution !

Study of the Rayleigh-Bénard system: dimensionless model

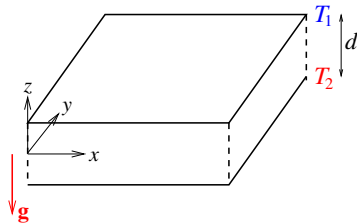
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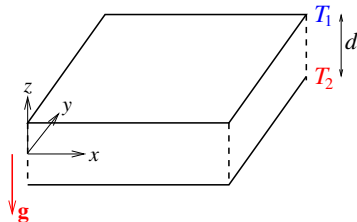
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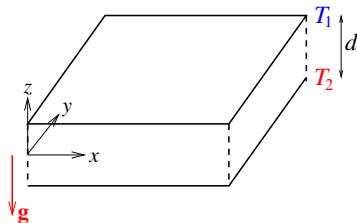
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with the **Rayleigh number** $R = \alpha \delta T g d^3 / (\kappa \nu)$ and the **Prandtl number** $P = \nu / \kappa$.

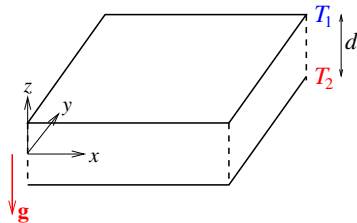
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Isotropy of the problem in the horizontal plane \Rightarrow focus on **2D** xz solutions

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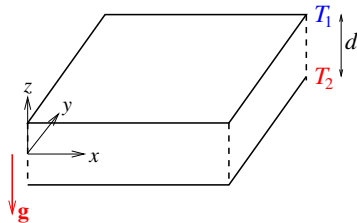
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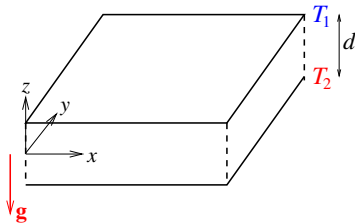
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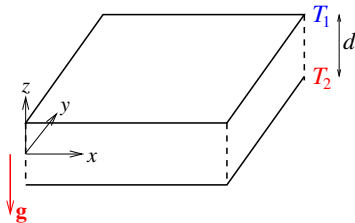
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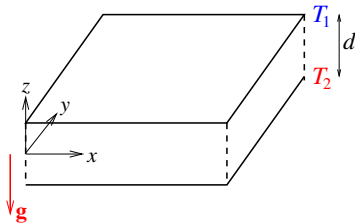
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How can one eliminate p in (NS)? Consider $\operatorname{curl}(\text{NS}) \cdot \mathbf{e}_y$ i.e. the **vorticity equation**:

$$P^{-1} \partial_t(-\Delta \psi) + P^{-1} [\partial_z(\mathbf{v} \cdot \nabla v_x) - \partial_x(\mathbf{v} \cdot \nabla v_z)] = -R \partial_x \theta + \Delta(-\Delta \psi). \quad (\text{VortE})$$

Study of 2D xz solutions of the Rayleigh-Bénard problem

Local state vector: $V = (\psi, \theta)$ s. t.

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obeys the system of coupled P.D.E.

$$D \cdot \partial_t V = L_R \cdot V + N_2(V, V)$$

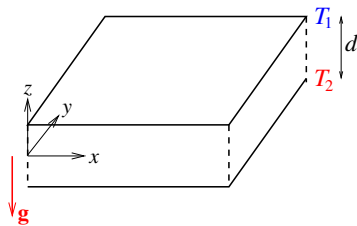
with D , L_R linear, N_2 nonlinear **differential operators**. 1st eq. is the **vorticity equation**:

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Study of 2D xz solutions of the Rayleigh-Bénard problem

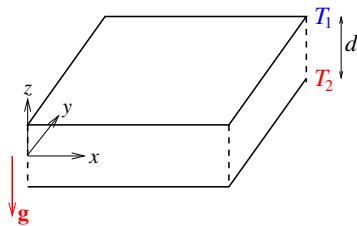
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What do we need to close this system ?

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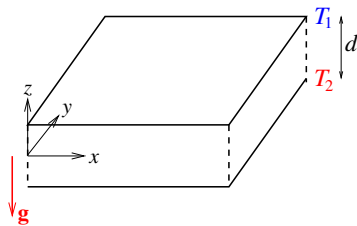
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What do we need to close this system ? Boundary conditions !

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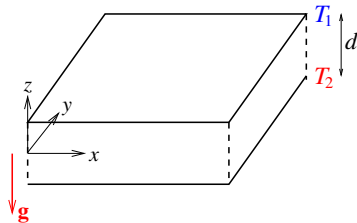
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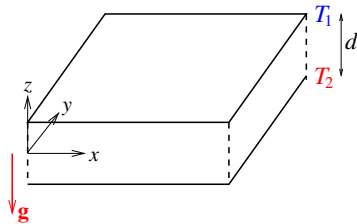
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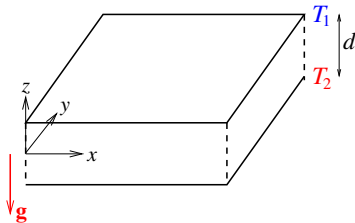
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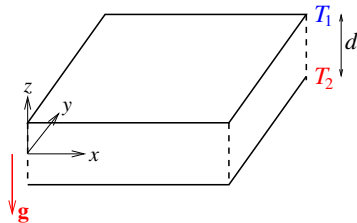
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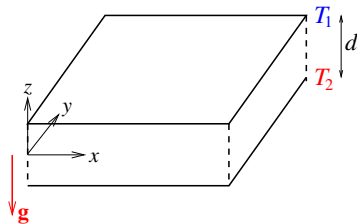
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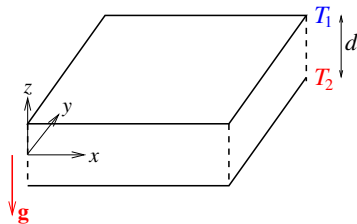
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or slip boundaries: $v_z = 0$ i.e. $\partial_x \psi = 0$ if $z = \pm 1/2$ **without shear stress !**

Shear stresses or tangential stresses

Come only from **viscous stresses**.

In physical units, the **viscous stress vector**

$$\mathbf{T} = \boldsymbol{\tau} \cdot \mathbf{n}$$

with the **viscous stress tensor**

$$\boldsymbol{\tau} = 2\eta\mathbf{S}$$

and the **rate-of-strain tensor**

$$\mathbf{S} = \frac{1}{2}(\nabla\mathbf{v} + \nabla\mathbf{v}^T),$$

\mathbf{n} the unit vector normal to the boundary, pointing outward.

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Come only from **viscous stresses**.

In physical units, the **viscous stress vector**

$$\mathbf{T} = \boldsymbol{\tau} \cdot \mathbf{n}$$

with the **viscous stress tensor**

$$\boldsymbol{\tau} = 2\eta\mathbf{S}$$

and the **rate-of-strain tensor**

$$\mathbf{S} = \frac{1}{2}(\nabla\mathbf{v} + \nabla\mathbf{v}^T),$$

\mathbf{n} the unit vector normal to the boundary, pointing outward.

Here

$$\mathbf{v} = -(\partial_z\psi)\mathbf{e}_x + (\partial_x\psi)\mathbf{e}_z$$

and

$$\mathbf{n} = \mp\mathbf{e}_z$$

$$\implies \text{Shear stress } T_x = \mp\eta(\partial_z v_x + \partial_x v_z) \quad \text{if } z = \pm 1/2.$$

Shear stresses or tangential stresses

Come only from **viscous stresses**.

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Since $v_z = 0$, $T_x = 0$ at the boundaries $\iff \partial_z v_x = 0$ if $z = \pm 1/2$.

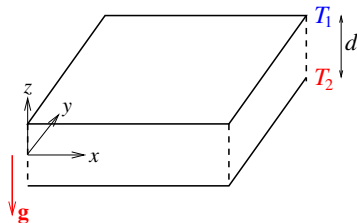
Study of 2D xz solutions of the Rayleigh-Bénard problem

Local state vector: $V = (\psi, \theta)$ s. t.

$$\mathbf{v} = -(\partial_z \psi) \mathbf{e}_x + (\partial_x \psi) \mathbf{e}_z,$$

$$T = T_0 - z + \theta,$$

$$\boxed{D \cdot \partial_t V = L_R \cdot V + N_2(V, V)},$$



$$[D \cdot \partial_t V]_\psi = P^{-1}(-\Delta \partial_t \psi), \quad [L_R \cdot V]_\psi = -R \partial_x \theta + \Delta(-\Delta \psi), \quad (\text{VortE})$$

$$[N_2(V, V)]_\psi = P^{-1}[\partial_x(\mathbf{v} \cdot \nabla v_z) - \partial_z(\mathbf{v} \cdot \nabla v_x)], \quad (\text{VortE})$$

$$[D \cdot \partial_t V]_\theta = \partial_t \theta, \quad [L_R \cdot V]_\theta = \Delta \theta + v_z, \quad [N_2(V, V)]_\theta = -\mathbf{v} \cdot \nabla \theta. \quad (\text{HE})$$

Boundary conditions on θ : **Isothermal boundaries:** $\theta = 0$ if $z = \pm 1/2$.

Boundary conditions on ψ i.e. \mathbf{v} :

Slip boundaries: $v_z = 0$ and $\partial_z v_x = 0 \iff \partial_x \psi = \partial_z^2 \psi = 0$ if $z = \pm 1/2$.

Extended geometry in the xy plane: no B.C. or periodic B.C. under $x \mapsto x + L$.

Linear stability analysis of the 2D xz Rayleigh-Bénard problem

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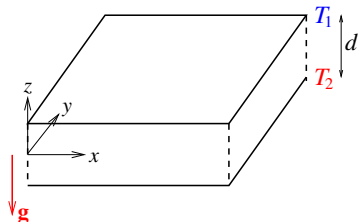
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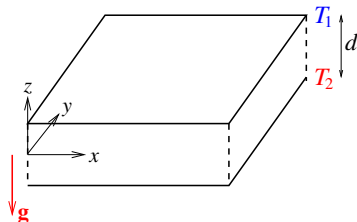
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Ex. 1.1: Normal mode analysis: the solution of the initial value problem is the superposition of normal modes that are Fourier modes in $\exp(ikx)$,

$$V = V_1(k, N) \exp[\sigma(k, N) t] \quad \text{with} \quad V_1(k, N) = (\widehat{\Psi}(z), \widehat{\Theta}(z)) \exp(ikx),$$

$k =$ **horizontal wavenumber**, $k \neq 0$, N another label to mark normal modes, $\sigma(k, N)$ the **temporal eigenvalue**.

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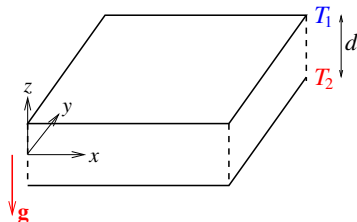
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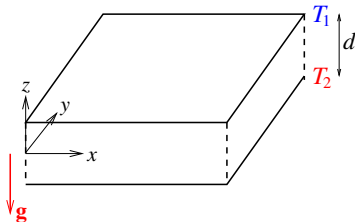
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$$\partial_x \psi = \partial_z^2 \psi = \theta = 0 \quad \text{if} \quad z = \pm 1/2.$$



Ex. 1.1: Generalized eigenvalue problem solved by normal modes analysis: most relevant normal modes are Fourier modes in $\exp(ikx)$ and have a z -profile in $\cos(\pi z)$,

$$V = V_1(k, N) \exp[\sigma(k, N) t] \quad \text{with} \quad V_1(k, N) = (\Psi, \Theta) \exp(ikx) \cos(\pi z),$$

$k =$ **horizontal wavenumber**, $k \neq 0$, N another label to mark normal modes, $\sigma(k, N)$ the **temporal eigenvalue**.

They satisfy the boundary conditions: $\hat{\Psi} = \hat{\Psi}'' = 0, \quad \hat{\Theta} = 0 \quad \text{if} \quad z = \pm 1/2.$